

Direct Geometrico-Static Problem of Underconstrained Cable-Driven Parallel Robots with 5 Cables

Ghasem Abbasnejad and Marco Carricato

Abstract The direct geometrico-static problem of cable-driven parallel robots with 5 cables is presented. The study provides procedures for the identification of all equilibrium poses of the end-effector when cable lengths are assigned. A least-degree univariate polynomial in the ideal governing the problem is obtained, thus showing that the latter has 140 solutions in the complex field. By a continuation technique, an upper bound on the number of real solutions is estimated. An algorithm based on parameter homotopy continuation is developed for the efficient computation of the whole solution set, including equilibrium poses with slack cables.

Key words: Cable-driven robots, underconstrained robots, kinematics, statics.

1 Introduction

Cable-driven parallel robots (CDPRs) use cables instead of rigid-body legs to control the end-effector (EE) pose. CDPRs are *underconstrained* when the number of cables in tension (namely, *active*) is smaller than the number of degrees of freedom that the EE possesses with respect to the base. In this case, only some freedoms may be controlled, and the EE configuration depends on the applied forces, e.g. gravity [13]. The displacement analysis of these robots requires the simultaneous solution of both loop-closure and equilibrium equations. As a consequence, the *direct geometrico-static problem* (DGP), which aims at finding all equilibrium poses of the EE when cable lengths are assigned, is especially challenging [10, 12].

When the cable lengths of a CDPR with n cables, $n \leq 6$, are assigned as inputs, the number of active cables at the equilibrium is, a priori, unknown. Indeed, the EE may reach an equilibrium pose with one or more cables being slack. Since multiple

Ghasem Abbasnejad and Marco Carricato
Dept. of Industrial Engineering & Interdept. Center for Health Sciences and Technologies
University of Bologna, Italy, e-mail: marco.carricato@unibo.it.

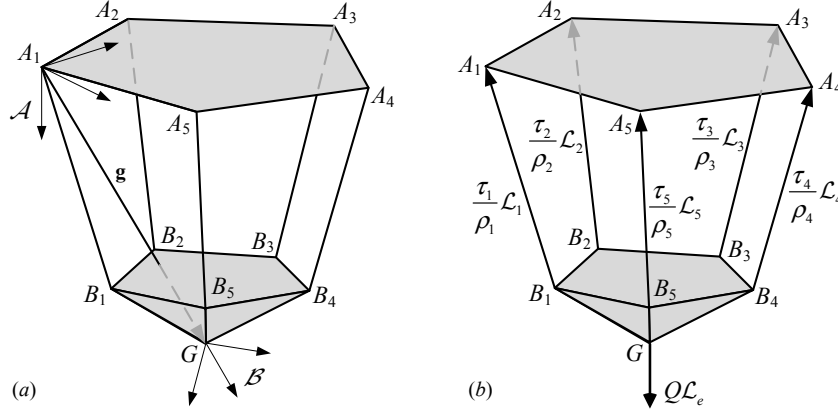


Fig. 1 A CDPR with 4 cables: geometric model (a) and static model (b).

stable configurations may exist, possibly characterized by different numbers of taut cables, the robot may switch between them because of inertia forces or external disturbances. Accordingly, the computation of the whole solution set for a given DGP is essential for robust trajectory planning.

The authors have solved so far the DGP of robots with 2, 3 and 4 active cables [5, 3, 4]. These problems were proven to admit 24, 156 and 216 solutions in the complex field, respectively. The DGP of a CDPR suspended by 6 cables admits 40 solutions, since it is equivalent to the forward displacement analysis of the Gough platform [11]. The present contribution shows that the DGP of a CDPR with 5 active cables admits 140 solutions in the complex field, and it also estimates an upper bound on the number of real configurations. Parameter homotopy continuation is used to develop an efficient algorithm to determine the whole solution set. The results reported in the paper complete the authors' study concerning the DGP of underconstrained CDPRs with generic geometry.

2 Geometrico-static model

The EE is connected to a fixed base by 5 cables, which are modeled as inextensible and massless (Fig. 1). The i th cable, $i = 1 \dots 5$, is assigned length ρ_i , it exits from the base at point A_i , and it is connected to the EE at point B_i . \mathcal{A} is a fixed Cartesian coordinate frame with origin at A_1 , and \mathcal{B} is a Cartesian frame attached to the EE at point G . The EE pose is described by $\mathbf{X}^T = [\mathbf{g}^T; \Phi^T]$, where $\mathbf{g}^T = [x, y, z]^T$ is the position of G in \mathcal{A} , and $\Phi^T = [e_1, e_2, e_3]^T$ is the array grouping the Rodrigues parameters parameterizing the EE orientation with respect to \mathcal{A} . The EE is acted upon by force $Q\mathcal{L}_e$, where Q is a constant magnitude and \mathcal{L}_e is the normalized Plücker vector of the force line of action, passing through G and parallel to direction

\mathbf{k} , without loss of generality. The normalized Plücker vector of line $A_i B_i$ is \mathcal{L}_i/ρ_i , where $\mathcal{L}_i^T = [(A_i - B_i)^T; \{(A_i - A_1) \times (A_i - B_i)\}^T]$. If τ_i is the intensity of the cable tensile force, the wrench exerted by the i th cable on the EE is $(\tau_i/\rho_i) \mathcal{L}_i$, and static equilibrium may be expressed as

$$\sum_{i=1}^5 \frac{\tau_i}{\rho_i} \mathcal{L}_i + Q \mathcal{L}_e = \underbrace{[\mathcal{L}_1 \ \mathcal{L}_2 \ \mathcal{L}_3 \ \mathcal{L}_4 \ \mathcal{L}_5 \ \mathcal{L}_e]}_{\mathbf{M}} \begin{bmatrix} (\tau_1/\rho_1) \\ (\tau_2/\rho_2) \\ (\tau_3/\rho_3) \\ (\tau_4/\rho_4) \\ (\tau_5/\rho_5) \\ Q \end{bmatrix} = \mathbf{0}. \quad (1)$$

If *all* cables are active, the following 5 geometrical constraints must be satisfied:

$$q_i := \|A_i - B_i\|^2 - \rho_i^2 = 0, \quad i = 1 \dots 5, \quad (2)$$

Equations (1) and (2) amount to 11 scalar relations in 11 variables, namely \mathbf{X} and τ_i , $i = 1 \dots 5$. Following Refs. [5], cable tensions may be eliminated from the set of unknowns by observing that Eq. (1) holds only if

$$p := \det \mathbf{M} = 0, \quad (3)$$

which is a purely geometrical condition, since \mathbf{M} only depends on \mathbf{X} . Equations (2) and (3) amount to 6 relations in 6 pose coordinates. Polynomials q_1, \dots, q_5 in Eq. (2) have degree 4 in \mathbf{X} , whereas polynomial p in Eq. (3) has degree 9 in \mathbf{X} . The 0-dimensional variety V of the ideal $\langle J \rangle$ generated by the set $J = \{q_1, \dots, q_5, p\}$ yields the solutions of the DGP at hand.

3 Problem-solving algorithm

Like in the studies concerning the DGP of robots suspended by 2, 3 and 4 cables [5, 3, 4], a formal proof about the number of solutions contained in V is provided by implementing an elimination procedure based on Groebner bases and Sylvester dialytic method. Then, a numerical algorithm based on homotopy continuation is presented to compute the solution set in an efficient way.

3.1 The elimination approach

In order to ease numeric computation via a computer algebra system, namely the GroebnerPackage provided within the software Maple15, all geometric parameters of the robot are assigned generic *rational values*. Accordingly, $\langle J \rangle \subset \mathbb{Q}[\mathbf{X}]$, where $\mathbb{Q}[\mathbf{X}]$ is the set of all polynomials in \mathbf{X} with coefficients in \mathbb{Q} . All Groeb-

ner bases are computed with respect to graded reverse lexicographic monomial orders (grevlex, in brief), which provide the most efficient calculations. In general, a Groebner basis $G[J]$ of $\langle J \rangle$ with respect to $\text{grevlex}(\mathbf{X})$, with variables ordered so that $z > y > x > e_1 > e_2 > e_3$, may be computed in a fairly expedited way. For instance, for the robot reported in Table 1, `Maple` computes $G[J]$ in roughly 3.3min, on a PC with a 2.67GHz Intel Xeon processor and 4GB of RAM.

Once $G[J]$ is known, the normal set $\mathbf{N}[J]$ of $\langle J \rangle$, i.e. the set of all monomials that are *not* multiples of any leading monomial in $G[J]$, may be easily computed. Since $\mathbf{N}[J]$ comprises 140 monomials, this is also the number of complex roots in V and, thus, the order of the least-degree univariate polynomials of $\langle J \rangle$ [14]. Any one of these polynomials may be computed by the hybrid approach proposed in [3], based on the cooperative use of the FGLM algorithm [9] and a dialytic procedure similar to that presented in [7].

If \mathbf{X}_l is a list of l variables in \mathbf{X} and $\mathbf{X} \setminus \mathbf{X}_l$ is the relative complement of \mathbf{X}_l in \mathbf{X} , a monomial order $>_l$ on $\mathbb{Q}[\mathbf{X}]$ is of l -elimination type provided that any monomial involving a variable in \mathbf{X}_l is greater than any monomial in $\mathbb{Q}[\mathbf{X} \setminus \mathbf{X}_l]$. If $G_{>_l}[J]$ is a Groebner basis of $\langle J \rangle$ with respect to $>_l$, then $G[J_l] := G_{>_l}[J] \cap \mathbb{Q}[\mathbf{X} \setminus \mathbf{X}_l]$ is a basis of the l th elimination ideal $\langle J_l \rangle := \langle J \rangle \cap \mathbb{Q}[\mathbf{X} \setminus \mathbf{X}_l]$ [6]. The FGLM algorithm may be conveniently used to convert $G[J]$ from $\text{grevlex}(\mathbf{X})$ to $>_l$, so that $G[J_l]$ may be readily isolated from $G_{>_l}[J]$. In particular, the FGLM algorithm may be used to compute the Groebner basis $G[J_3]$ of $\langle J_3 \rangle$, where the latter is the set of polynomials of $\langle J \rangle$ that contain monomials in e_1, e_2 and e_3 only. Eliminating more unknowns by the FGLM algorithm is not convenient, since memory usage and computation time exponentially increase with l . A more efficient alternative emerges by computing a Sylvester-type eliminant matrix from the polynomials of $G[J_3]$. Since $G[J_3]$ comprises 31 polynomials and 31 monomials in e_1 and e_2 , if e_3 is assigned the role of ‘hidden’ variable, the generators of $G[J_3]$ may be set up as

$$\mathbf{T}(e_3)\mathbf{E} = \mathbf{0}, \quad (4)$$

where $\mathbf{T}(e_3)$ is a 31×31 matrix polynomial in e_3 , and \mathbf{E} is a vector grouping the 31 monomials in $G[J_3]$ with variables in $\{e_1, e_2\}$. As expected, letting the determinant of $\mathbf{T}(e_3)$ vanish yields a spurious-root-free polynomial of degree 140 in e_3 .

Sylvester dialytic elimination may be applied to the Groebner basis of *any* elimination ideal $\langle J_l \rangle$ of $\langle J \rangle$. However, the smaller l , the higher the order of the eliminant matrix, and the more onerous the expansion of its determinant. Accordingly, the fewer variables are eliminated by the FGLM algorithm, the smaller the computation burden of the FGLM step, but the more demanding the Sylvester elimination. Numerical experimentation seems to indicate that the elimination of x, y and z by the FGLM algorithm, and successively of e_1 and e_2 by a dialytic step, provides the best compromise. The `Maple` implementation of the above procedure is able to compute the univariate polynomial in e_3 for the example reported in Table 1 in roughly 610min, which is a substantial achievement for a polynomial of order 140.

3.2 Numerical computation of the solution set

The univariate polynomial obtained in Section 3.1 is important under a theoretical viewpoint, but it has a too high degree for a practical use. For the numerical calculation of the solution set, homotopy continuation provides a more robust and efficient alternative. In this perspective, the complexity and degree of polynomial p in Eq. (3) are a disadvantage, since they slow down computation and cause stability problems (cf. [4]). For this reason, the formulation of static equilibrium via Eq. (1) and a new parametrization of the EE pose are preferable.

Without loss of generality, unit vectors \mathbf{u} , \mathbf{v} and \mathbf{w} of the coordinates axes of \mathcal{B} may be chosen so that \mathbf{u} is directed from G to B_1 , \mathbf{v} lies in plane GB_1B_2 , and $\mathbf{w} = \mathbf{u} \times \mathbf{v}$. If $[\mathbf{u}]_{\mathcal{A}} = [u_1, u_2, u_3]$ and $[\mathbf{v}]_{\mathcal{A}} = [v_1, v_2, v_3]$ are the projections of \mathbf{u} and \mathbf{v} in the fixed frame, the platform pose may be written as a function of the 9 variables $x, y, z, u_1, u_2, u_3, v_1, v_2,$ and v_3 , which must satisfy the conditions

$$q_6 := \mathbf{u}^T \mathbf{u} - 1 = 0, \quad q_7 := \mathbf{v}^T \mathbf{v} - 1 = 0, \quad q_8 := \mathbf{u}^T \mathbf{v} = 0. \quad (5)$$

Equations (1), (2) and (5) form a system I of 14 scalar equations in 14 variables, i.e.

$$\mathbf{Y} = [x, y, z, u_1, u_2, u_3, v_1, v_2, v_3, \tau_1, \tau_2, \tau_3, \tau_4, \tau_5]^T. \quad (6)$$

Though I involves more variables and more equations than J , it comprises simpler lower-order polynomials, which are stabler when homotopy continuation is implemented, thus leading to a faster computation. In particular, polynomials q_1 and q_2 in Eq. (2) and q_6, q_7 and q_8 in Eq. (5) have degree 2 in \mathbf{Y} ; q_3, q_4 and q_5 in Eq. (2) have degree 4 in \mathbf{Y} ; and all polynomials in Eq. (1) have degree 3 in \mathbf{Y} . On the basis of these degrees, the problem at hand may be cast into the larger family of systems made up by 5 quadratic, 6 cubic and 3 quartic equations on $\mathbf{Y} \in \mathbb{P}^{14}$. By counting solutions at infinity, a general member of this family has a number of isolated roots equal to the minimal multi-homogeneous Bezout number [14]. This is also the number of paths tracked by the homotopy-continuation software used in this paper, i.e. Bertini [2]. By searching all possible multi-homogenizations, the minimal Bezout number emerges when \mathbf{Y} is partitioned as $[\{x, y, z, u_1, u_2, u_3\}, \{v_1, v_2, v_3\}, \{\tau_1, \tau_2, \tau_3, \tau_4, \tau_5\}]$, and it is equal to 11520.

When the isolated roots of the DGP of a generic robot are known, *parameter-homotopy continuation* [14] may be used to find the solutions for any other DGP of the same kind, in an efficient way. Since the coefficients of the equations in I are continuous functions of the geometric parameters \mathbf{P} of the robot, a continuous path through parameter space determines a continuous evolution of the coefficients and, generally, continuous paths for the solutions as well. Accordingly, if the 140 isolated roots of I are known for a generic $\mathbf{P} = \mathbf{P}_0$, the solutions for any other \mathbf{P} may be found by tracking the homotopy

$$I(\mathbf{Y}, (1-t)\mathbf{P}_0 + t\mathbf{P}) = \mathbf{0}, \quad (7)$$

Table 1 Real equilibrium configurations with nonnegative cable tensions of a 5-cable robot with: $\mathbf{a}_1 = [0, 0, 0]$, $\mathbf{a}_2 = [1, 2, -0.75]$, $\mathbf{a}_3 = [3.5, 1, 1]$, $\mathbf{a}_4 = [3.25, -1, 1]$, $\mathbf{a}_5 = [1, -2, -.5]$, $\mathbf{b}_1 = [-1, 0, -1]$, $\mathbf{b}_2 = [-.5, 1, -1.25]$, $\mathbf{b}_3 = [0.75, 0.75, -1.25]$, $\mathbf{b}_4 = [0.5, -.75, -1.25]$, $\mathbf{b}_5 = [-0.25, -0.8, -1.5]$, $(\rho_1, \rho_2, \rho_3, \rho_4, \rho_5) = (4.5, 5, 3, 3.75, 4.75)$, $Q = 10$ and $\mathbf{k} = [0, 0, 1]$.

No.	(x, y, z)	(e_1, e_2, e_3)	$(\tau_1, \tau_2, \tau_3, \tau_4, \tau_5)$	\mathbf{H}_r
1	1.4589, -1.2145, 2.4744	30.8167, 76.5978, -18.4146	1.73, 0.66, 0.62, 1.72, 6.44,	<
2	1.4441, -1.3000, 2.4723	14.9565, 39.3587, -10.5282	2.85, 0, 0.03, 2.75, 5.75,	<
3	1.4227, -1.2821, 2.4725	19.3442, 45.2411, -12.2058	2.87, 0.10, 0, 2.70, 5.72,	<
4	1.2273, -0.1010, 1.8629	30.4252, -1.1058, -3.3465	0, 5.27, 0.99, 0, 6.37,	<>
5	2.3443, 1.0649, 2.1627	4.5139, 5.2434, 1.4044	0, 6.95, 3.15, 1.97, 0,	<>
6	1.4384, -1.2969, 2.4722	15.5535, 39.7125, -10.6817	2.91, 0, 0, 2.78, 5.71,	<
7	2.4803, 0.5613, 1.8416	53.8079, -123.9777, -16.1938	5.78, 0, 7.44, 0, 1.20,	<>
8	2.1463, 0.2983, 5.3178	-0.1057, 0.0133, -0.0550	3.18, 0, 5.48, 0, 1.65,	>
9	2.2516, 0.3107, 4.0816	-0.0967, -0.5150, 15.2829	4.75, 0, 6.96, 0, 3.96,	<>
10	2.6647, 1.2853, 2.0725	7.4388, 42.2955, 13.4023	0.61, 5.33, 5.77, 0, 0,	<>
11	2.5662, -0.1206, 1.4236	35.9962, -26.9853, 3.5481	0, 0, 7.04, 0, 8.28,	<>
12	1.0000, -0.0768, 1.8522	19.0651, 1.5022, -2.5059	0, 6.27, 0, 0, 6.21,	<>
13	2.6694, 1.3323, 2.0672	5.7677, 19.8499, 6.4974	0, 5.94, 5.60, 0, 0,	<>
14	2.4243, 0.6927, 1.8269	-19.0280, 57.3828, 10.2733	7.05, 0, 7.66, 0, 0,	<>

with t varying from 0 to 1 or, more robustly, along the curve $t = \gamma t' / [1 + (\gamma - 1)t']$, with $t' \in [0, 1]$ and $\gamma \in \mathbb{C}$. In this case, only 140 paths need to be tracked, and paths corresponding to solutions at infinity are avoided. By this approach, Bertini converges to the solutions of the example reported in Table 1 in roughly 4.28min (with the default settings). Among these solutions, only 2 are real, and only 1 has positive tension in all cables. The latter solution is listed in row 1 of Table 1.

3.3 Maximum number of real-valued solutions

The DGP of a CDPR suspended by 5 cables has 140 solutions in the complex field. However, since some roots may remain complex no matter how robot parameters are varied, the maximal number of real solutions may be smaller than 140. Determining a tight bound for this count is a challenging task. By a continuation procedure originally proposed by Dietmaier [8], and recently adapted by the authors to the DGP of underconstrained CDPRs [1], several sets of geometric parameters for which the DGP provides at the most 74 real configurations have been found so far. An example is as follows: $\mathbf{a}_2 = [1.44417, 0, 1.20333]$, $\mathbf{a}_3 = [0.302415, 1.26206, 0.55533]$, $\mathbf{a}_4 = [-0.711127, 0.808726, 0.810451]$, $\mathbf{a}_5 = [0.749568, 0.761578, -0.469085]$, $\mathbf{b}_1 = [2.16169, 0, 0]$, $\mathbf{b}_2 = [-0.125711, 0, 1.32615]$, $\mathbf{b}_3 = [-0.412791, 0.0211425, 0.449869]$, $\mathbf{b}_4 = [-0.16265, -0.468249, -0.399945]$, $\mathbf{b}_5 = [1.59653, 1.31446, 0.96224]$, $(\rho_1, \rho_2, \rho_3, \rho_4, \rho_5) = (2.46449, 1.99586, 1.20622, 1.42395, 2.4302)$.

4 Equilibrium configurations with unloaded cables

When cable lengths are assigned as inputs, nothing ensures, a priori, that when the EE reaches its stable equilibrium pose all cables are in tension, since configurations may exist in which the EE is supported by only m cables, with $m \leq 5$ and $5 - m$ cables being slack. Accordingly, the overall solution set emerges by solving the DGP for all possible constraint sets $\{\|A_j - B_j\| = \rho_j, j \in \mathcal{W}\}$, with $\mathcal{W} \subseteq \{1, 2, 3, 4, 5\}$ and $\text{card}(\mathcal{W}) \leq 5$. Clearly, when the k th cable is slack, the distance $\|A_k - B_k\|$ cannot be greater than the assigned ρ_k . Hence, for any subset \mathcal{W} , only the solutions for which $\|A_k - B_k\| \leq \rho_k$, for all $k \notin \mathcal{W}$, must be retained. In general, for a robot with 5 cables, 31 DGPs need to be solved, namely 1 DGP with 5 active cables, 5 DGPs with 4 active cables, 10 DGPs with 3 active cables, 10 DGPs with 2 active cables, and 5 DGPs with 1 active cable.

Table 1 shows the overall results for an exemplifying geometry. Due to space limitations, only the real solutions with nonnegative tension in all cables are reported. These comprise 1 configuration with 5 cables in tension (row 1), 2 configurations with 4 cables in tension (rows 2 – 3), 7 configurations with 3 cables in tension (rows 4 – 10), and 4 configurations with 2 cables in tension (rows 11 – 14). Stability is assessed by means of a reduced Hessian matrix \mathbf{H}_r , as proposed in [5]. Symbols $>$, $<$ and $<>$ denote, respectively, a positive-definite, a negative-definite and an indefinite matrix. A solution is stable when \mathbf{H}_r is positive-definite. For the case at hand, the robot has a single stable configuration, with 3 cables in tension.

5 Conclusions

This paper studied the direct geometrico-static problem (DGP) of underconstrained cable-driven parallel robot with 5 cables. The task consists in finding all equilibrium configurations that are compatible with the assigned cable lengths. Since the equations governing the problem comprise both geometrical and static constraints, the DGP is a challenging task.

A least-degree univariate polynomial was numerically obtained by an elimination procedure, thus showing that 140 solutions exist in the complex field. A continuation algorithm was then developed to identify a robot geometry leading to the highest number of real equilibrium configurations. A bound of 74 real configurations was estimated. After the solutions with nonnegative tension in all cables are sifted and stability is considered, the number of feasible configurations decreases remarkably.

For the efficient computation of the whole solution set, including configurations with slack cables, an algorithm based on parameter homotopy continuation was developed. The algorithm is the foundation of the software DGP – Solver, which is currently being developed by the authors to automatize the computation of all equilibrium configurations of a CDPR with an arbitrary number of cables.

References

- [1] Abbasnejad, G., Carricato, M.: Real solutions of the direct geometrico-static problem of under-constrained cable-driven parallel robots with 3 cables: a numerical investigation. *Meccanica* **47**(7), 1761–1773 (2012)
- [2] Bates, D.J., Hauenstein, J.D., Sommese, A.J., Wampler, C.W.: Bertini: Software for numerical algebraic geometry. Available at <http://www.nd.edu/~sommese/bertini>
- [3] Carricato, M.: Direct geometrico-static problem of underconstrained cable-driven parallel robots with three cables. *ASME Journal of Mechanisms and Robotics*, to appear (2013)
- [4] Carricato, M., Abbasnejad, G.: Direct geometrico-static analysis of underconstrained cable-driven parallel robots with 4 cables. In: T. Bruckmann, A. Pott (eds.) *Cable-Driven Parallel Robots*, pp. 269–285. Springer-Verlag, Berlin Heidelberg (2013)
- [5] Carricato, M., Merlet, J.P.: Stability analysis of underconstrained cable-driven parallel robots. *IEEE Transactions on Robotics* **29**(1), 288–296 (2013)
- [6] Cox, D., Little, J., O’Shea, D.: *Ideals, varieties, and algorithms*. Springer, New York (2007)
- [7] Dhingra, A.K., Almadi, A.N., Kohli, D.: A Gröbner-Sylvester hybrid method for closed-form displacement analysis of mechanisms. *ASME Journal of Mechanical Design* **122**(4), 431–438 (2000)
- [8] Dietmaier, P.: The Stewart-Gough platform of general geometry can have 40 real postures. In: J. Lenarčič, M.L. Husty (eds.) *Advances in Robot Kinematics: Analysis and Control*, pp. 7–16. Kluwer Academic Publishers, Dordrecht (1998)
- [9] Faugère, J.C., Gianni, P., Lazard, D., Mora, T.: Efficient computation of zero-dimensional Gröbner bases by change of ordering. *Journal of Symbolic Computation* **16**(4), 329–344 (1993)
- [10] McCarthy, J.M.: 21st century kinematics: synthesis, compliance, and tensegrity. *ASME Journal of Mechanisms and Robotics* **3**(2), 020201/1–3 (2011)
- [11] Merlet, J.P.: *Parallel robots*. Springer, Dordrecht (2006)
- [12] Merlet, J.P.: Wire-driven parallel robot: open issues. In: V. Padois, P. Bidaud, O. Khatib (eds.) *Romansy 19 – Robot Design, Dynamics and Control*, pp. 3–10. Springer, Vienna (2013)
- [13] Ming, A., Higuchi, T.: Study on multiple degree-of-freedom positioning mechanism using wires—Part 1: Concept, design and control. *Int. Journal of the Japan Society for Precision Engineering* **28**(2), 131–138 (1994)
- [14] Sommese, A.J., Wampler, C.W.: *The numerical solution of systems of polynomials arising in engineering and science*. World Scientific Publishing, Singapore (2005)